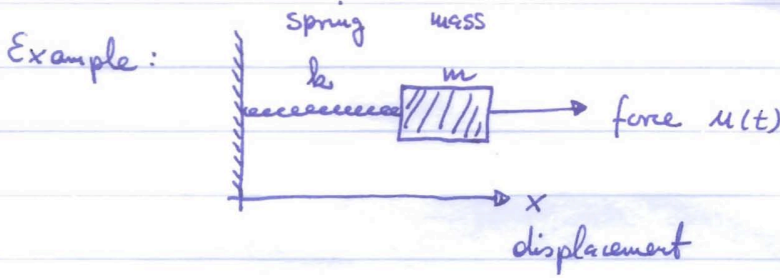


Class #12

Cross-Spectral Analysis (linear system theory)



input : force $u(t)$

output : displacement $x(t)$

system parameters : spring constant k
mass - " - m

balance of forces $u(t) + u_s(t) + u_m(t) = 0$

$u_s(t) = -k x(t)$ $u_m(t) = -m \ddot{x}(t)$ inertia = mass * acceleration
restoring force of spring

$m \ddot{x} + kx = u$ ~~F~~ mass * acceleration = sum of all forces
(inertia) (external applied + spring)



What's the "transfer" function that transforms the input $u(t)$ to the output $x(t)$?

What's the response of the system to an input

$$X(f) = H(f) \cdot U(f)$$

for unit impulse, i.e., $u(t) = \delta(t)$, $\mathcal{F}(\delta(t)) = 1$

\downarrow $X(f) = H(f) \cdot 1$ definition of transfer func.

$$\mathcal{F}(m\ddot{x} + kx = u(t))$$

$$\downarrow [-m(2\pi f)^2 + k] \cdot X(f) = U(f)$$

unit impulse as input, that is $u(t) = \delta(t) \quad \downarrow \mathcal{F}(u(t)) = 1$

$$\downarrow [-m(2\pi f)^2 + k] \cdot H(f) = 1$$

$$\downarrow H(f) = [k - m(2\pi f)^2]^{-1}$$

resonance for
 $k = m(2\pi f_c)^2$
 or $f_c = \sqrt{\frac{k}{m}} \cdot \frac{1}{2\pi}$

→ Tacoma Bridge Video
 instantaneous response

no phase lag (in this special case) as $H(f)$ is real,
 however, this is not generally the case, i.e.,
 consider a "damping" term in the spring system:
 (linear friction)

$$\mathcal{F}(m\ddot{x} + r\dot{x} + kx = u(t))$$

$$\downarrow [-m(2\pi f)^2 + rj(2\pi f) + k] \cdot H(f) = 1 \quad u(t) = \delta(t)$$

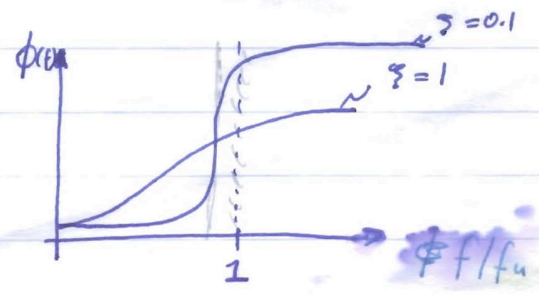
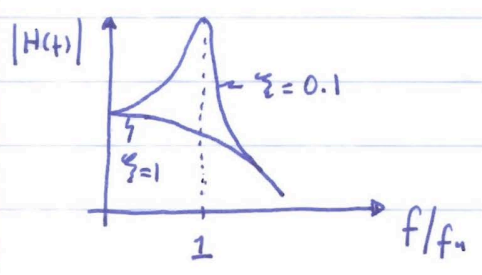
$$\downarrow H(f) = \frac{1/k}{1 - (f/f_n)^2 + j 2\zeta(f/f_n)}$$

"natural" or "resonance" frequency
 $f_n = \frac{1}{2\pi} \sqrt{k/m}$

$$\zeta = \frac{r}{2} \sqrt{\frac{1}{km}}$$

or $H(f) = |H(f)| e^{-j\phi(f)}$

polar notation



76

Cross-spectral analysis is not really interested directly in the system but rather in its input/output relationships, i.e., we are interested in the system's response that we infer from measurements of the

input: $x(t)$

output: $y(t)$

Cross-Covariance

[how much variance in $y(t)$ is explained by the variance of $x(t)$?]

we will construct
transfer functions

↳ this

$$R_{xy}(\tau) = E[x(t)y(t+\tau)] = \iint_{-\infty}^{\infty} x(t)y(t+\tau)p(x,y)dx dy$$

$$= \lim_{N \rightarrow \infty} \frac{1}{N} \sum_{k=1}^N x_k(t) y_k(t+\tau)$$

ergodic, stationary process

$$= \lim_{T \rightarrow \infty} \frac{1}{T} \int_0^T x(t)y(t+\tau) d\tau$$

$R_{xy}(\tau)$ can carry both signs

$$\max(R_{xy}(\tau)) \neq R_{xy}(\tau=0)$$

$$R_{xy}(\tau) \neq R_{xy}(-\tau) \quad \text{not an even fctn., but}$$

$$R_{xy}(\tau) = R_{yx}(-\tau)$$

Cross-spectral density fctn.

$$S_{xy}(f) = \int_{-\infty}^{\infty} R_{xy}(\tau) e^{-j2\pi f\tau} d\tau$$

is the FFT of $R_{xy}(\tau)$ and is complex, but

$$S_{xy}(-f) = S_{xy}^*(f) = S_{yx}(f) \quad \text{complex valued}$$

$$S_{xx}(-f) = S_{xx}^*(f) = S_{xx}(f) \quad \text{real valued}$$

Define one sided cross-spectra

$$G_{xy} = \begin{cases} 2S_{xy} & f > 0 \\ 0 & f \leq 0 \end{cases}$$

$$G_{xy}(f) = C_{xy}(f) - j Q(f) \\ = 2 \int_{-\infty}^{\infty} R_{xy} \cos(2\pi ft) dt - 2j \int_{-\infty}^{\infty} R_{xy} \sin(2\pi ft) dt$$

co-spectrum

quadrature spectrum

One can also write

$$G_{xy}(f) = |G_{xy}(f)| e^{j\phi_{xy}(f)}$$

where

$$|G_{xy}(f)| = \sqrt{C_{xy}^2 + Q_{xy}^2}$$

$$\phi_{xy}(f) = \tan^{-1} \left(\frac{Q_{xy}(f)}{C_{xy}(f)} \right)$$

Cross-spectral analysis allows to assess the linear relation (correlation) between two time series for each frequency separately. It also allows to analyse the phase relations between the two series.

$$\text{If } Q_{xy} = 0 \quad \& \quad \phi_{xy} = 0 \quad \& \quad G_{xy} = |G_{xy}| = C_{xy}$$

and the two series are said to be in-phase

Def.: Coherence $\Gamma_{xy}^2(f)$

$$\Gamma_{xy}^2(f) = \frac{|G_{xy}(f)|^2}{G_{xx}(f) \cdot G_{yy}(f)}$$

is a direct (normalised) measure of the amount of variance of $y(t)$ that is linearly related to the variance in $x(t)$. It is equivalent to the time domain cross-correlation coefficient

$$r_{12}^2 = \frac{\left(\sum_{i=1}^N x_1 x_2 \right)^2}{\sum_{i=1}^N x_1^2 \sum_{i=1}^N x_2^2}$$

In the "real" world we have estimates only, i.e.,

$$\hat{G}_{xy}(t) = \hat{C}_{xy}(t) - j \hat{Q}_{xy}(t)$$

$$\hat{G}_{xy}(t) = \frac{2}{T} X^* \cdot Y$$

$$\tilde{F}(x(t)) = X(t) = A_x + j B_x = a_x e^{j\phi_x}$$

$$\tilde{F}(y(t)) = Y(t) = A_y + j B_y = a_y e^{j\phi_y}$$

$$\phi_x = \tan^{-1}(B_x/A_x) \quad a_x = (A_x^2 + B_x^2)^{1/2}$$

$$\phi_y = \tan^{-1}(B_y/A_y) \quad a_y = (A_y^2 + B_y^2)^{1/2}$$

$$G_{xy} = \frac{2}{T} X^* Y = \frac{2}{T} \left[(A_x A_y + B_x B_y) - j (A_y B_x - A_x B_y) \right]$$

$\hat{C}_{xy} \qquad \qquad \qquad \hat{Q}_{xy}$

$$\text{Now } \hat{\phi}_{xy}(t) = \tan^{-1} \frac{\hat{Q}_{xy}}{\hat{C}_{xy}} = \tan^{-1} \left(\frac{A_y B_x - A_x B_y}{A_x A_y + B_x B_y} \right)$$

$$\begin{aligned} \tan \hat{\phi}_{xy} &= \frac{\frac{A_y B_x}{A_x A_y} - \frac{A_x B_y}{A_x A_y}}{1 + \frac{B_x B_y}{A_x A_y}} = \frac{\tan \hat{\phi}_x - \tan \hat{\phi}_y}{1 + \tan \hat{\phi}_x \tan \hat{\phi}_y} \\ &= \tan(\hat{\phi}_x - \hat{\phi}_y) \end{aligned}$$

$\hat{\phi}_{xy}$ measures the relative phase or the phase difference between the input $x(t)$ and the output $y(t)$

$$\hat{\phi}_{xy} = \hat{\phi}_x - \hat{\phi}_y$$

SUMMARY

A linear process between input and output is completely described by

- (1) its coherence Γ_{xx}^2
- (2) its phase $\hat{\phi}_{xy}$
- (3) its amplitude or modulus $|G_{xy}|$

But we get estimates only, i.e.,

$$\hat{\Gamma}_{xy}^2 = \frac{(X^* Y) \cdot (X Y^*)}{X^* X \cdot Y^* Y} \equiv 1$$

↑
no "smoothing" done yet
"raw" estimates with
2 d.o.f.

We need

$$\overline{\hat{\Gamma}_{xy}^2} = \frac{|\overline{\hat{G}_{xy}}|^2}{\overline{\hat{P}_x} \overline{\hat{P}_y}} \neq 1$$

go to p. 86
for estimation
of confidence levels

end class #12

↑ Not much is known on the distributional properties of this → **EMPIRICAL**