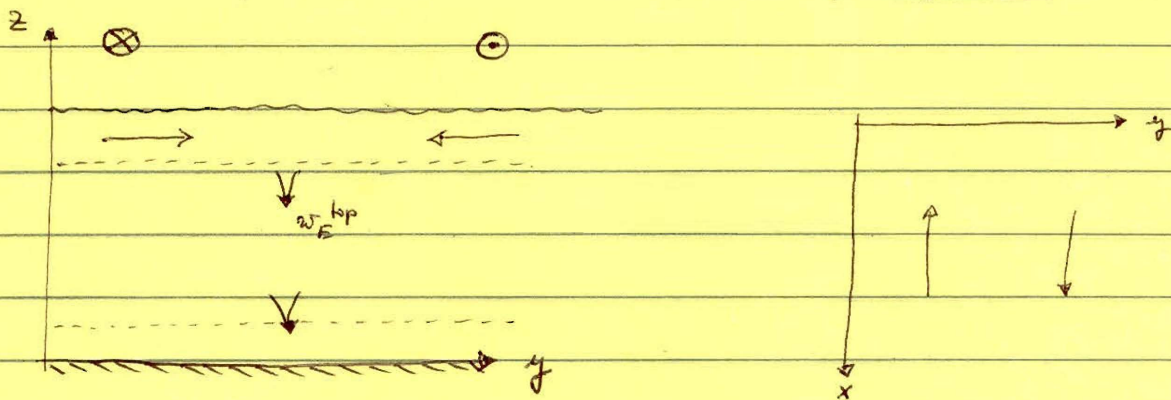


Large Scale Ocean Circulation (steady state)



$$w_E^{top} = \frac{\partial}{\partial x} \left(\frac{\tau^y}{\rho f} \right) - \frac{\partial}{\partial y} \left(\frac{\tau^x}{\rho f} \right)$$

Ekman pumping
due to wind-stress curl

$$w_E^{bottom} = \frac{f}{|f|} \frac{d}{dz} \left(\frac{\partial v_g}{\partial x} - \frac{\partial u_g}{\partial y} \right)$$

Ekman pumping
due to bottom friction

For the geostrophic interior, we have $[u_g = u, v_g = v]$

$$\begin{cases} -(f_0 + \beta_0 y) v = -\frac{1}{\rho} \frac{\partial p}{\partial x} & | \frac{\partial}{\partial y} \\ + (f_0 + \beta_0 y) u = -\frac{1}{\rho} \frac{\partial p}{\partial y} & | \frac{\partial}{\partial x} \end{cases} \quad \beta = \beta_0 L / f_0 \ll 1$$

notice that there is NO vertical dependence!

$$\sigma = -\frac{1}{\rho_0} \frac{\partial p}{\partial z}$$

↳ $\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y}$ does not depend on z either nor does, by inference $\frac{\partial w}{\partial z}$!

$$\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} + \frac{\partial w}{\partial z} = \sigma$$

linearised continuity equation

taking the curl of momentum

$$f_0 \left(\frac{\partial u}{\partial x} + \frac{\partial v}{\partial y} \right) + \beta_0 v = \sigma \quad \rightarrow \quad f_0 \frac{\partial w}{\partial z} = \beta_0 v$$

No vertical dependence in (x, y, z) momentum

$\hookrightarrow (u, v, w)$ do not depend on z !

$$\hookrightarrow \frac{\partial w}{\partial z} = \frac{w_E^{\text{top}} - w_E^{\text{bottom}}}{H}$$

$$\frac{\partial w}{\partial z} = \frac{1}{\rho f_0 H} \vec{k} \cdot \nabla \times \vec{\tau} - \frac{d}{2H} \frac{f_0}{|f_0|} \xi_g$$

geostrophic rel. vorticity:

$$\xi_g = \frac{\partial w}{\partial x} - \frac{\partial u}{\partial y} = \frac{1}{\rho f_0} \nabla^2 p$$

linearized
 ∇
 into the vorticity equation which is

geostrophic velocity $\vec{v} = \frac{1}{\rho f_0} \nabla p$

2nd derivative of pressure

$$\frac{\partial w}{\partial z} = \frac{\beta_0 \vec{v}}{f_0} = \frac{\beta_0}{f_0} \frac{1}{\rho f_0} \frac{\partial p}{\partial x}$$

and we get

$$\frac{1}{\rho f_0 H} (\vec{k} \cdot \nabla \times \vec{\tau}) - \frac{d}{2H} \frac{f_0}{|f_0|} \frac{1}{\rho f_0} \nabla^2 p - \frac{\beta_0}{f_0^2 \rho} \frac{\partial p}{\partial x} = 0$$

wind-stress curl
 (surface Ekman)

relative vorticity
 (bottom Ekman)

vortex stretching
 (planetary β -effect)

$$\text{or } \frac{d}{2H} \frac{|f_0|}{\rho f_0} \nabla^2 p + \frac{\partial p}{\partial x} = \frac{1}{\rho f_0 H} f_0^2 \vec{k} \cdot \nabla \times \vec{\tau}$$

relative vorticity

β -effect

known forcing (curl of wind) vorticity

$$\text{or } \frac{d}{2H} \frac{|f_0|}{\rho \beta_0} \nabla^2 p + \frac{\partial p}{\partial x} = \frac{1}{H} \frac{f_0}{\beta_0} \vec{k} \cdot \nabla \times \vec{\tau}$$

bottom Ekman layer

beta-effect

surface Ekman layer

ocean gyre
 western boundary
 current
 Stommel + Stredrup

$$\beta = \frac{\beta_0 L}{f_0}$$

$$\frac{\text{relative vorticity}}{\beta\text{-effect}} = \frac{\frac{d|f|}{2H\beta_0} \nabla^2 p}{\frac{\partial p}{\partial x}} \sim \frac{d}{H} \cdot \frac{1}{\beta} = \frac{E_v^{1/2}}{\beta} \approx 0.02$$

$$\left. \begin{array}{l} \text{turbulence-enhanced viscosity } A \sim 10^{-2} \text{ m}^2 \text{ s}^{-1} \\ f_0 \sim 10^{-4} \text{ s}^{-1} \\ H \sim 3000 \text{ m} \end{array} \right\} \rightarrow d \sim 15\text{-m} \quad \left(\frac{d}{|f|} \right)^{1/2}$$

$$\frac{d}{H} \sim 0.005$$

$$\left. \begin{array}{l} \beta_0 \sim 2 \cdot 10^{-11} \text{ m}^{-1} \text{ s}^{-1} \\ L \sim 10^6 \text{ m} \end{array} \right\} \beta \sim 0.2 \quad \beta = \frac{\beta_0 L}{f_0}$$

↓

neglect relative vorticity (from bottom friction; small relative to β -effect)

$$\frac{\partial p}{\partial x} = \frac{f_0}{\beta_0 H} \left(\frac{\partial \tau^{(y)}}{\partial x} - \frac{\partial \tau^{(x)}}{\partial y} \right)$$

or

$$v = \frac{1}{\rho_0 \beta_0 H} \left(\frac{\partial \tau^{(y)}}{\partial x} - \frac{\partial \tau^{(x)}}{\partial y} \right)$$

neglect $\tau^{(x)}$ for case
of integration

Sverdrup (1947)

$$\text{or } p = P_2(y) - \frac{f_0}{\beta_0 H} \int_{k_1}^x \frac{\partial \tau^{(x)}}{\partial y} dx = P_1(y) - \frac{f_0}{\beta_0 H} \frac{\partial \tau^{(x)}}{\partial y} (x - k_1)$$

constant in x
wind-stress
and

and

$$u = -\frac{1}{f_0 \rho} \frac{\partial p}{\partial y} = -\frac{1}{f_0 \rho} \frac{\partial P_2}{\partial y} + \frac{f_0}{f_0 \beta_0 H} \frac{\partial}{\partial y} \int_{k_1}^x \frac{\partial \tau^{(x)}}{\partial y} dx$$